

CIVL7008 Seismic Analysis for Building Structures

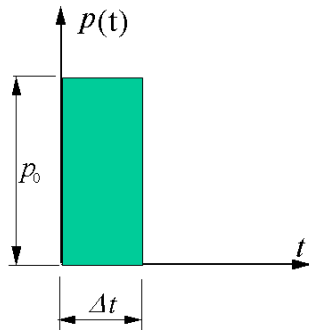
Lec-03 Forced Vibration of SDOF System



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Dr. Dino Chen

Force Vibration: Rectangle Impulse Excitation



$$I = p_0 \Delta t$$

$$m\ddot{v} + c\dot{v} + kv = 0$$

$$v(t) = e^{-\xi\omega t} \left[\frac{\dot{v}_0 + v_0 \xi \omega}{\omega_d} \sin \omega_d t + v_0 \cos \omega_d t \right]$$

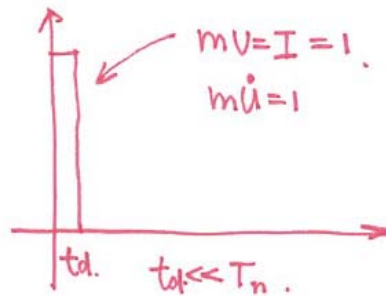
$$v_0 = 0, \quad \dot{v}_0 = \frac{p_0}{m} \Delta t$$

$$v(t) = e^{-\xi\omega t} \frac{p_0 \Delta t}{m \omega_d} \sin \omega_d t$$

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Rectangular Impulse



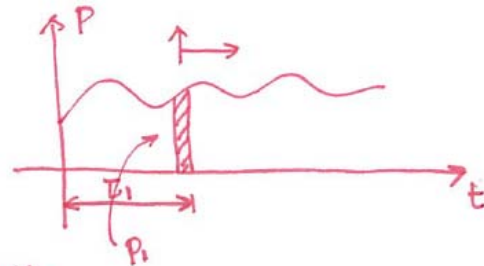
$$\begin{cases} \dot{u}(0) = \frac{1}{m} \\ u(0) = 0 \end{cases} \text{ initial condition.}$$

$$u(t) = u_0 \cos \omega_n t + \left(\frac{\dot{u}_0}{\omega_n} \right) \sin \omega_n t$$

$$u(t) = 0 + \left(\frac{1}{m \omega_n} \right) \sin \omega_n t \quad \text{For Undamped System.}$$

Damped System.

$$u(t) = \exp(-\xi \omega_n t) \cdot \frac{1}{m \omega_d} \cdot \sin \omega_d t.$$



Unit:

$$\begin{cases} u(t) = \exp[-\xi \omega_n (t - t_1)] \cdot \sin \omega_d (t - t_1) \cdot \frac{I}{m \omega_d} \\ I = P_i \cdot \Delta t \end{cases}$$

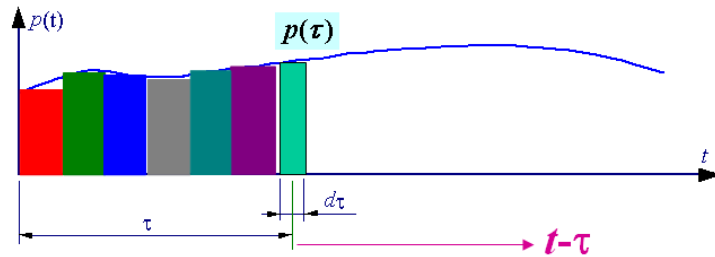
Particular Solution

$$u_p = \int_0^t \left\{ \frac{P(\tau)}{m \omega_d} \cdot \exp[-\xi \omega_n (t - \tau)] \cdot \sin \omega_d (t - \tau) \right\} d\tau$$

Duhamel Integration.

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From $v(t) = e^{-\xi\omega t} \frac{p_0 \Delta t}{m\omega_d} \sin \omega_d t$

$t \rightarrow t - \tau$
 $p_0 \rightarrow p(\tau)$
 $\Delta t \rightarrow d\tau$

$\Rightarrow dv(t) = \frac{p(\tau) d\tau}{m\omega_d} e^{-\xi\omega(t-\tau)} \sin \omega_d(t-\tau)$

$$v(t) = \int_0^t \frac{p(\tau)}{m\omega_d} e^{-\xi\omega(t-\tau)} \sin \omega_d(t-\tau) d\tau$$

Lec-03 Forced Vibration of SDOF System

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$$u_p = \int_0^t \left[\frac{p(\tau)}{m\omega_d} \cdot \exp(-\xi\omega(t-\tau)) \cdot \sin \omega_d(t-\tau) \right] d\tau$$

Damped - system.

$$= \int_0^t \left[\frac{p(\tau)}{m\omega_d} \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot [\sin \omega_d t * \cos \omega_d \tau - \cos \omega_d t * \sin \omega_d \tau] \right] d\tau$$

$$= \frac{1}{m\omega_d} \int_0^t p(\tau) \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot \omega_d \omega_d \tau \cdot \underbrace{\sin \omega_d t}_{\uparrow} d\tau - \frac{1}{m\omega_d} \int_0^t p(\tau) \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot \sin \omega_d \tau \cdot \underbrace{\cos \omega_d t}_{\uparrow} d\tau$$

$$= \sin \omega_d t \cdot \underbrace{\frac{1}{m\omega_d} \int_0^t p(\tau) \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot \omega_d \omega_d \tau \cdot d\tau}_{\leftarrow} - \cos \omega_d t \cdot \underbrace{\frac{1}{m\omega_d} \int_0^t p(\tau) \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot \sin \omega_d \tau \cdot d\tau}_{\rightarrow}$$

$$= \sin \omega_d t \cdot A - \cos \omega_d t \cdot B$$

$$A = \frac{1}{m\omega_d} \int_0^t p(\tau) \cdot \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot \omega_d \omega_d \tau \cdot d\tau$$

$$y = p(\tau) \cdot \cos \omega \tau$$

$$A = \frac{1}{m\omega_d} \int_0^t \frac{\exp(-\xi\omega\tau)}{\exp(-\xi\omega t)} \cdot y \cdot d\tau$$

Simple summation:

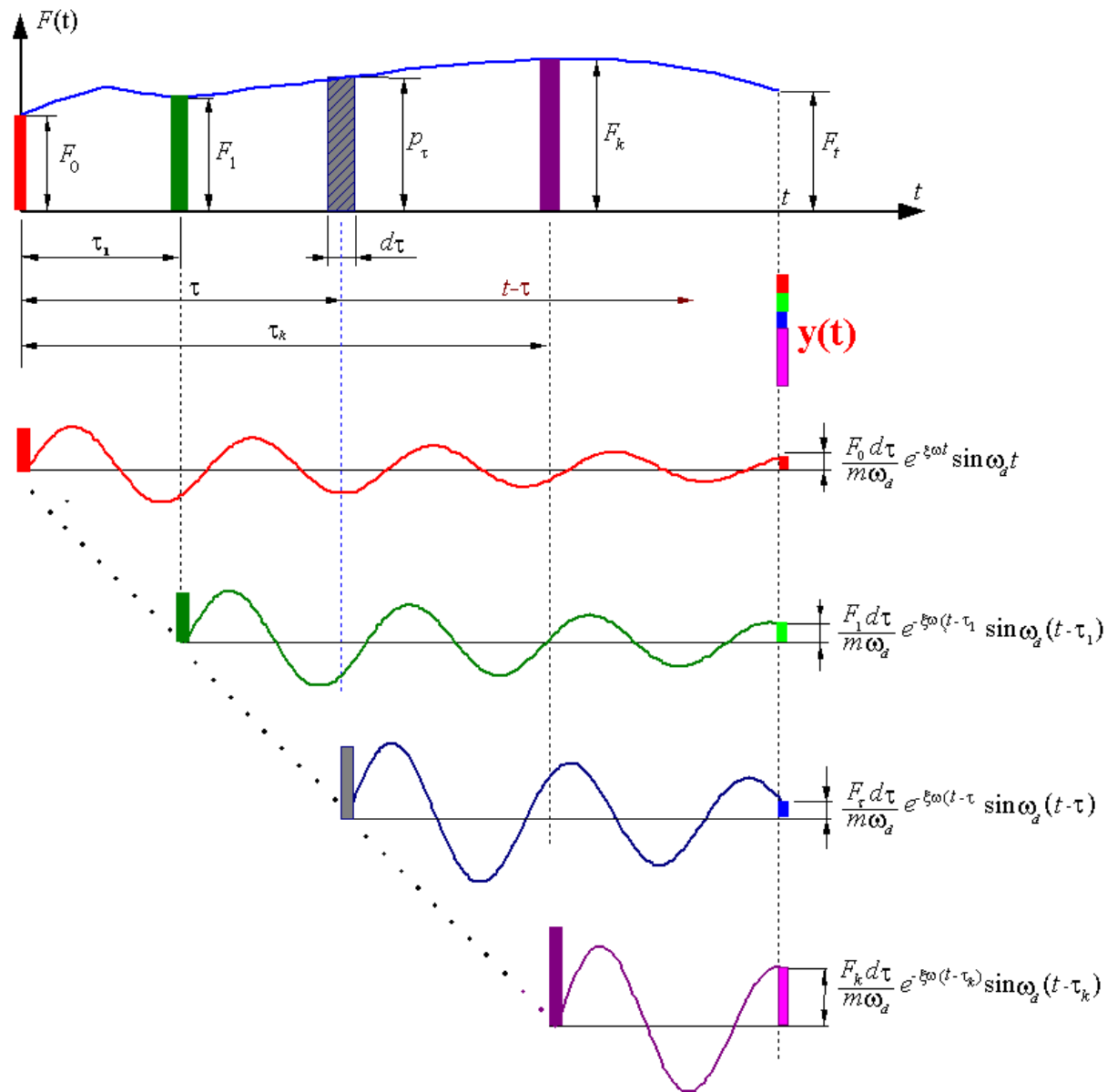
$$\bar{A}_N = \bar{A}_{N-1} \cdot \exp(-\xi\omega\Delta\tau) + \frac{\Delta\tau}{m\omega} \cdot [y_{N-1}] \cdot \exp(-\xi\omega\Delta\tau)$$

Simpson's rule:

$$\bar{A}_N = \bar{A}_{N-2} \cdot \exp(-2\xi\omega\Delta\tau) + \frac{\Delta\tau}{3m\omega_d} \cdot [y_{N-2} \cdot \exp(-\xi\omega\Delta\tau \cdot 2) + 4y_{N-1} \cdot \exp(-\xi\omega\Delta\tau) + y_N]$$

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Excel Table for Duhamel Integration

$$v(t) = A(t) \sin \omega_D t - B(t) \cos \omega_D t$$

$$A(t) \equiv \frac{1}{m \omega_D} \int_0^t p(\tau) \frac{\exp(\xi \omega \tau)}{\exp(\xi \omega t)} \cos \omega_D \tau d\tau$$

$$B(t) \equiv \frac{1}{m \omega_D} \int_0^t p(\tau) \frac{\exp(\xi \omega \tau)}{\exp(\xi \omega t)} \sin \omega_D \tau d\tau$$

Simple summation:

$$A_N \doteq A_{N-1} \exp(-\xi \omega \Delta \tau) + \frac{\Delta \tau}{m \omega_D} y_{N-1} \exp(-\xi \omega \Delta \tau) \\ N = 1, 2, 3, \dots \quad (6-17a)$$

Trapezoidal rule:

$$A_N \doteq A_{N-1} \exp(-\xi \omega \Delta \tau) + \frac{\Delta \tau}{2 m \omega_D} \left[y_{N-1} \exp(-\xi \omega \Delta \tau) + y_N \right] \\ N = 1, 2, 3, \dots \quad (6-17b)$$

Simpson's rule:

$$A_N \doteq A_{N-2} \exp(-2 \xi \omega \Delta \tau) \\ + \frac{\Delta \tau}{3 m \omega_D} \left[y_{N-2} \exp(-2 \xi \omega \Delta \tau) + 4 y_{N-1} \exp(-\xi \omega \Delta \tau) + y_N \right] \\ N = 2, 4, 5, \dots \quad (6-17c)$$

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Excel Table for Duhamel Integration

TABLE E6-2
Numerical Duhamel integral analysis including damping

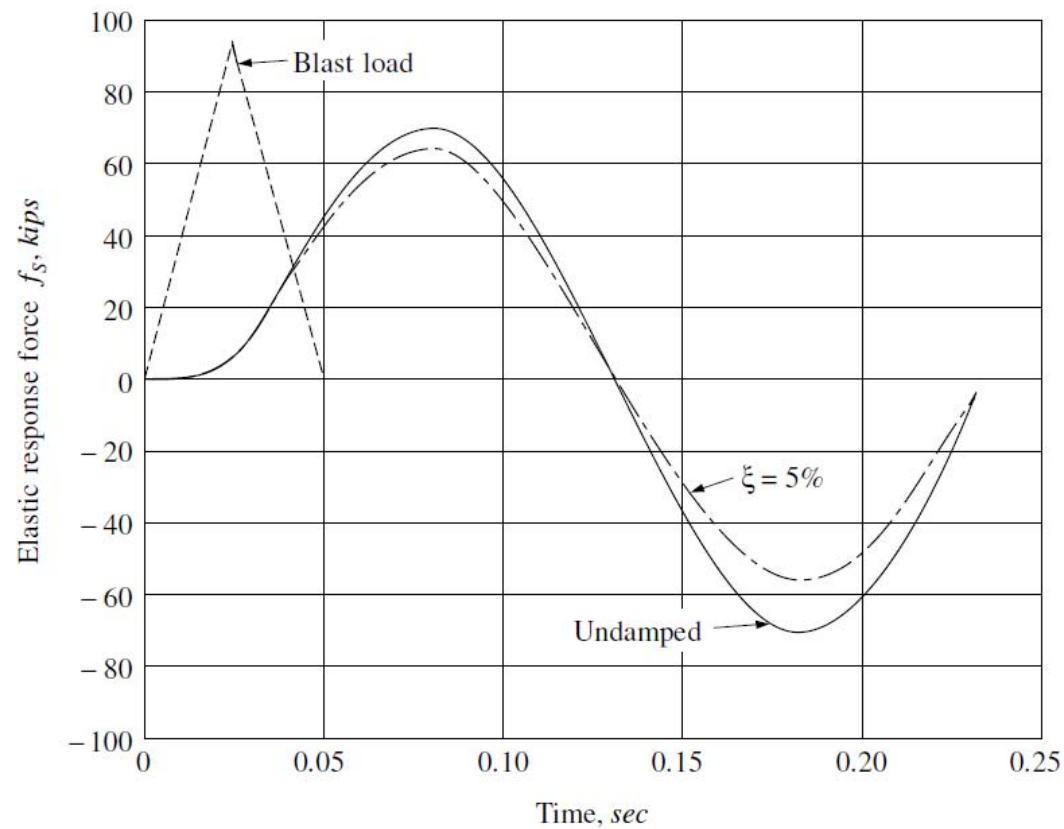
N	t_N sec	p_N kips (1)	$\sin 30 t_N$ (2)	$\cos 30 t_N$ (3)	y_N (1) × (3) kips (4)	y_{N-1} (5)	y_{N-2} (6)	$M_1 \times$ (5) (7)	$M_2 \times$ [(6) + (9)] (8)	$\frac{A_{N-2}}{F}$ (9)	$\frac{A_N}{F}$ (4) + (7) + (8) (10)	y_N (1) × (2) kips (11)	y_{N-1} (12)	y_{N-2} (13)	$M_1 \times$ (12) (14)	$M_2 \times$ [(13) + (16)] (15)	$\frac{B_{N-2}}{F}$ (16)	$\frac{B_N}{F}$ (11) + (14) + (15) (17)	(18)	(19)	(20)	v_N $F \times (20)$ ft (21)	$\int S_N$ $k \times (21)$ kips (22)
0	0.000	0	0	1.000	0	—	—	—	—	—	0	0	—	—	—	—	—	0	0	0	0	0	0
1	0.005	19.32	0.149	0.989	19.1	0	—	—	—	—	—	2.88	0	—	—	—	—	—	—	—	—	—	—
2	0.010	38.64	0.296	0.955	36.9	19.1	0	75.8	0	0	112.7	11.4	2.88	0	11.4	0	0	22.8	33.3	21.8	11.5	0.0002	0.58
3	0.015	57.96	0.435	0.900	52.2	36.9	19.1	—	—	—	—	25.2	11.4	2.88	—	—	—	—	—	—	—	—	—
4	0.020	77.28	0.565	0.825	63.8	52.2	36.9	207.2	147.4	112.7	418.4	43.7	25.2	11.4	100.0	33.7	22.8	177.4	236	146	90	0.0017	4.50
5	0.025	96.60	0.682	0.732	70.7	63.8	52.2	—	—	—	—	65.9	43.7	25.2	—	—	—	—	—	—	—	—	—
6	0.030	77.28	0.783	0.622	48.1	70.7	63.8	280.7	475.0	418.4	803.8	60.5	65.9	43.7	261.6	217.8	177.4	539.9	629	336	293	0.0054	14.65
7	0.035	57.96	0.867	0.498	28.9	48.1	70.7	—	—	—	—	50.3	60.5	65.9	—	—	—	—	—	—	—	—	—
8	0.040	38.64	0.932	0.362	14.0	28.9	48.1	114.7	839.1	803.8	967.8	36.0	50.3	60.5	199.7	591.4	539.9	827.1	902	299	603	0.0112	30.2
9	0.045	19.32	0.976	0.219	4.23	14.0	28.9	—	—	—	—	18.9	36.0	50.3	—	—	—	—	—	—	—	—	—
10	0.050	0	0.997	0.0707	0	4.23	14.0	16.8	967.1	967.8	983.9	0	18.9	36.0	75.0	850.1	827.1	925.1	981	65.4	915	0.0169	45.8
11	0.055	0	0.997	-0.0791	0	0	4.23	—	—	—	—	0	0	18.9	—	—	—	—	—	—	—	—	—
12	0.060	0	0.974	-0.227	0	0	0	0	969.1	983.9	969.1	0	0	0	0	911.2	925.1	911.2	900	-206	1106	0.0205	55.4
13	0.065	0	0.929	-0.370	0	0	0	—	—	—	—	0	0	0	—	—	—	—	—	—	—	—	—
14	0.070	0	0.863	-0.505	0	0	0	0	954.6	969.1	0	0	0	0	0	897.5	911.2	897.5	824	-453	1277	0.0236	63.9
15	0.075	0	0.778	-0.628	0	0	0	—	—	—	—	0	0	0	—	—	—	—	—	—	—	—	—
16	0.080	0	0.675	-0.737	0	0	0	0	940.3	954.6	940.3	0	0	0	0	884.0	897.5	884.0	635	-651.5	1286	0.0238	64.3
17	0.085	0	0.558	-0.830	0	0	0	—	—	—	—	0	0	0	—	—	—	—	—	—	—	—	—
18	0.090	0	0.427	-0.904	0	0	0	0	926.2	940.3	926.2	0	0	0	0	870.7	884.0	870.7	395	-787	1182	0.0219	59.1

$$\omega = \sqrt{\frac{kg}{W}} = 30 \text{ rad/sec} \quad \Delta\tau = 0.005 \text{ sec} \quad M_1 = 4 \exp(-\xi\omega\Delta\tau) = 3.97 \quad M_2 = \exp(-2\xi\omega\Delta\tau) = 0.985 \quad F = \frac{\Delta\tau}{3m\omega} = 1.852 \times 10^{-5} \text{ ft/kip} \quad k = 2700 \text{ kips/ft}$$

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Excel Table for Duhamel Integration

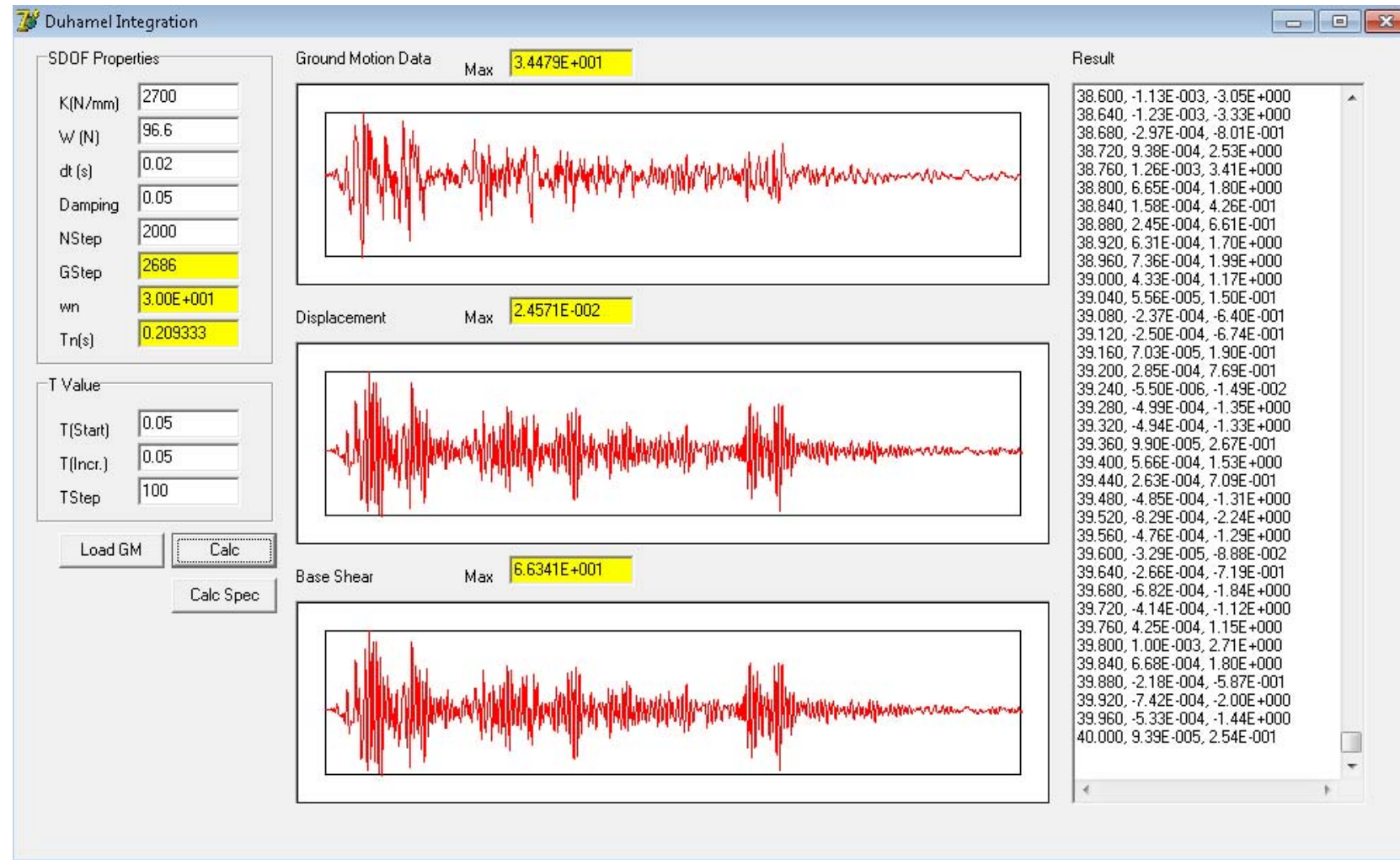
**FIGURE E6-2**

Response of water tower to blast load.

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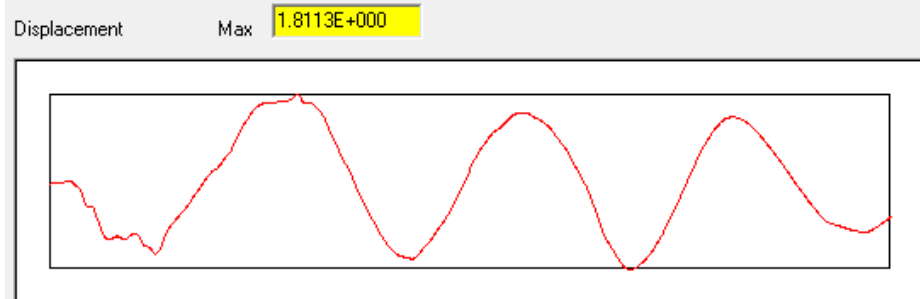
Program for Duhamel Integration (Solver For Force Vibration Problem of SDOF)



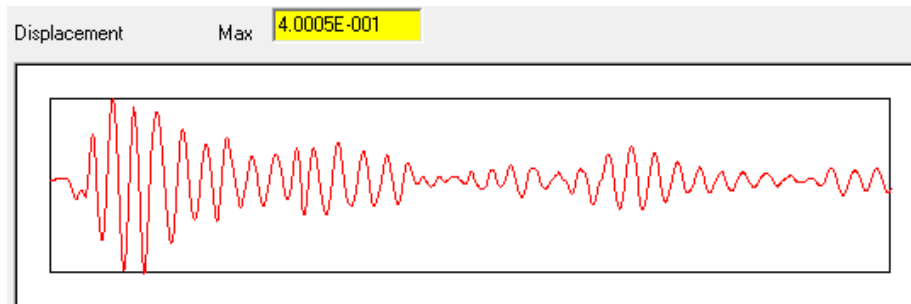
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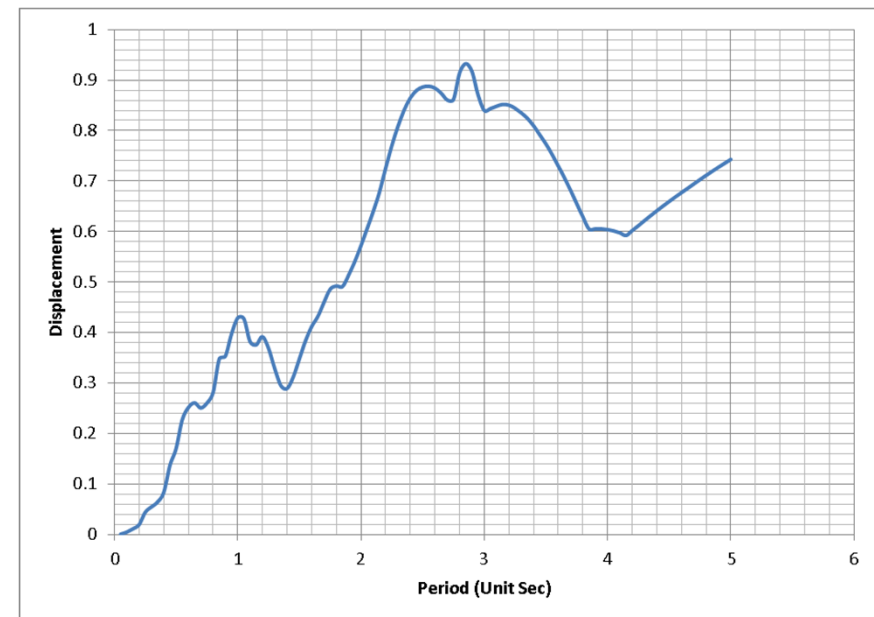
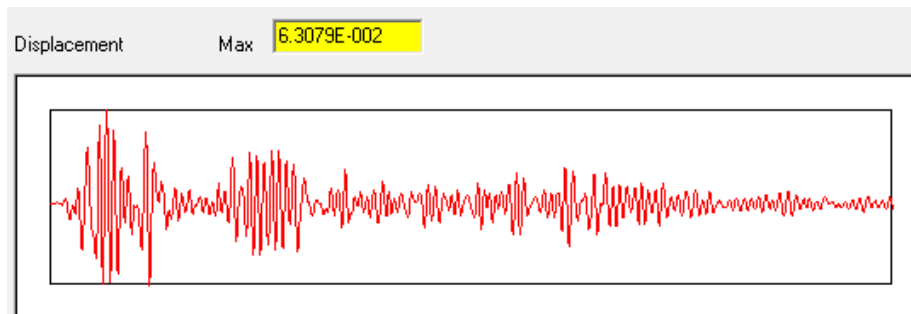
$K = 1, T_1 = 10.87 \text{ s}$



$K = 100, T_1 = 1.087 \text{ s}$



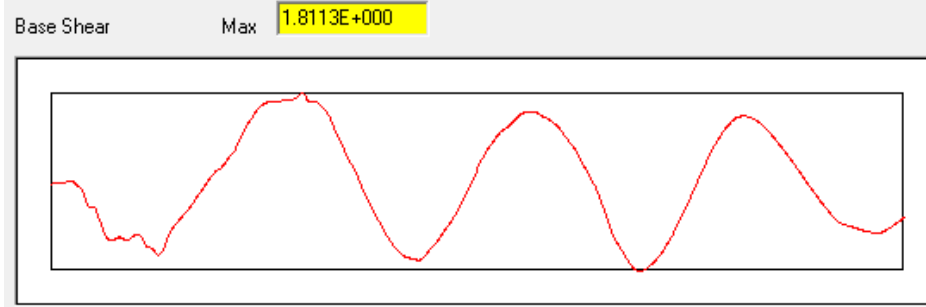
$K = 1000, T_1 = 0.344 \text{ s}$



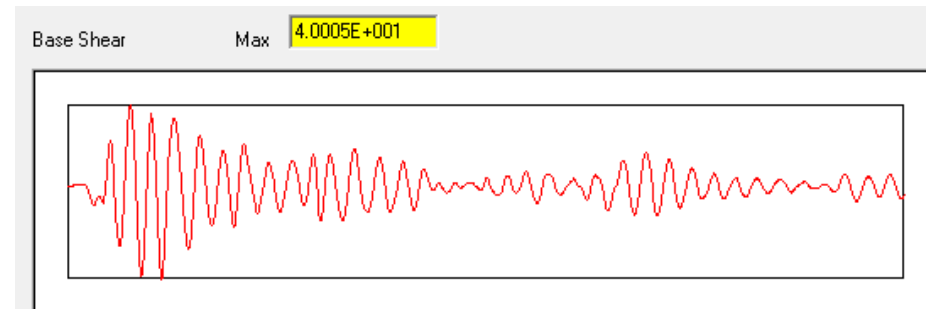
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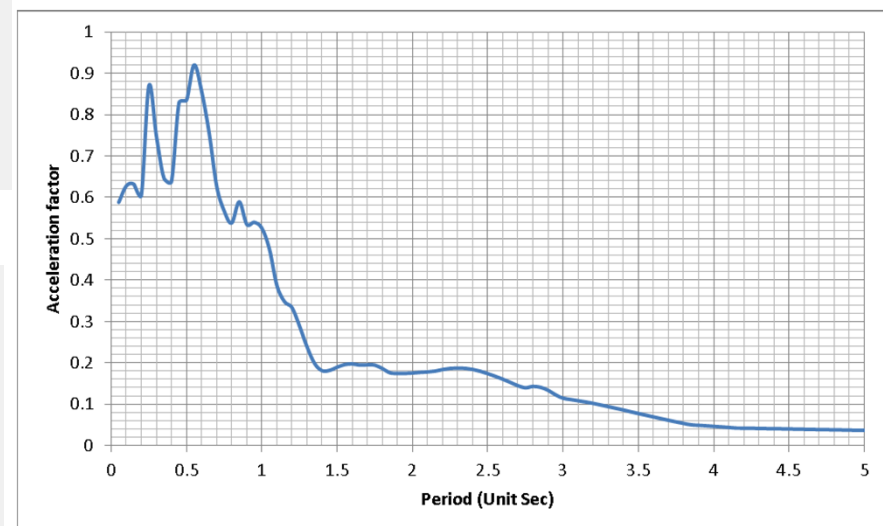
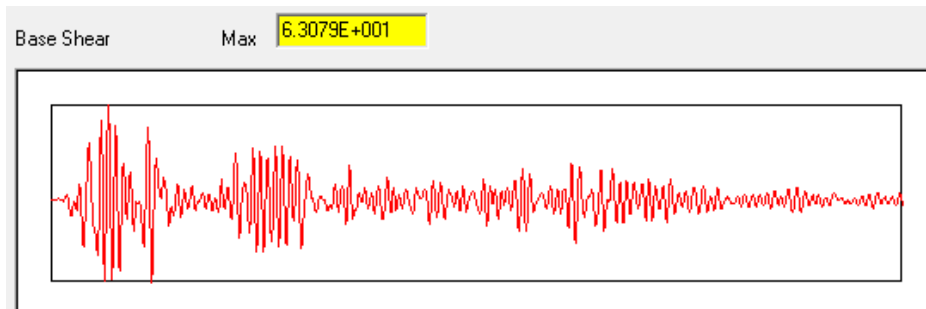
K = 1, T1 = 10.87 s



K = 100, T1 = 1.087 s



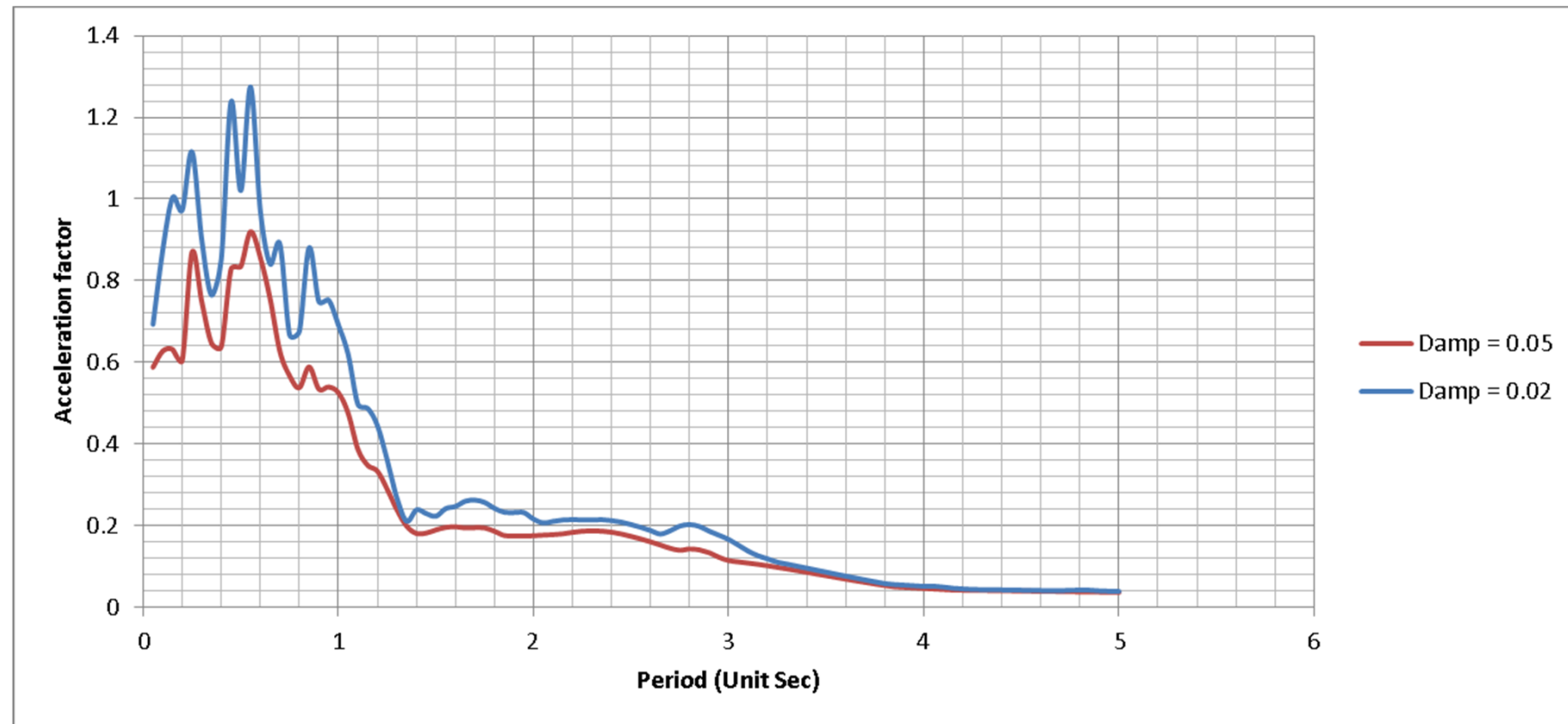
K = 1000, T1 = 0.344 s



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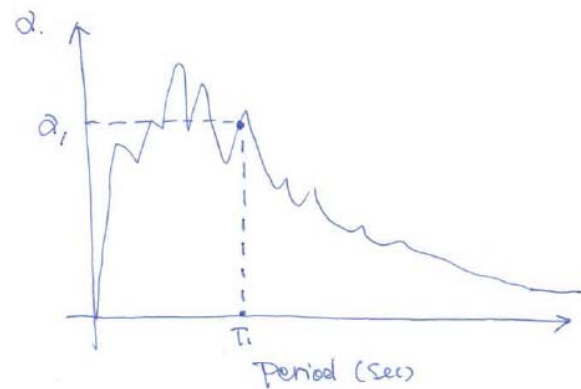
Spec Analysis From Duhamel Integration



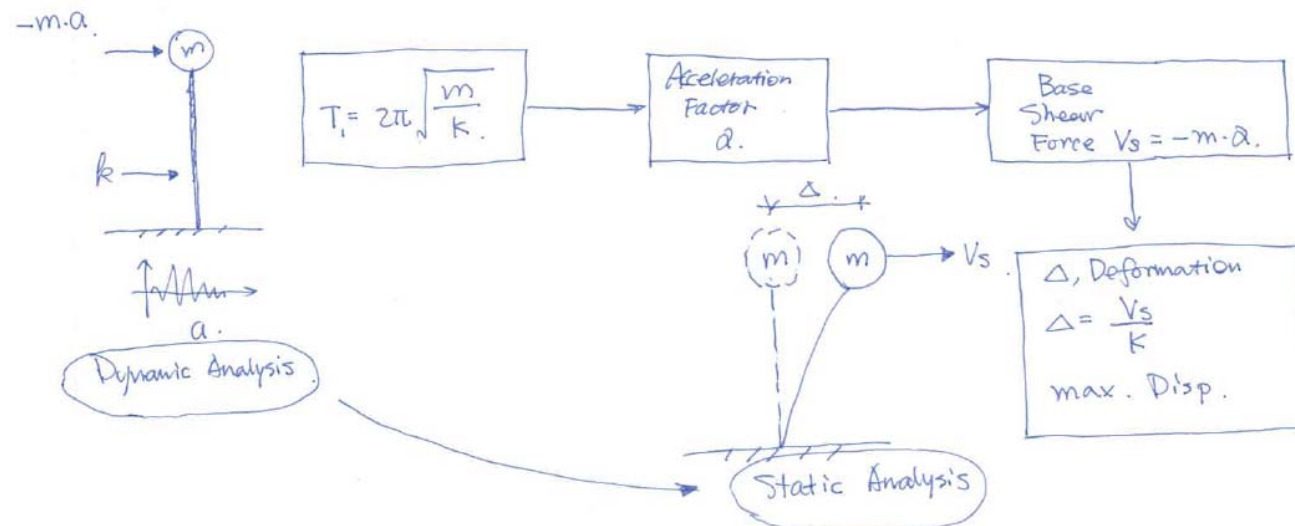
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Spec Analysis Simple Theory



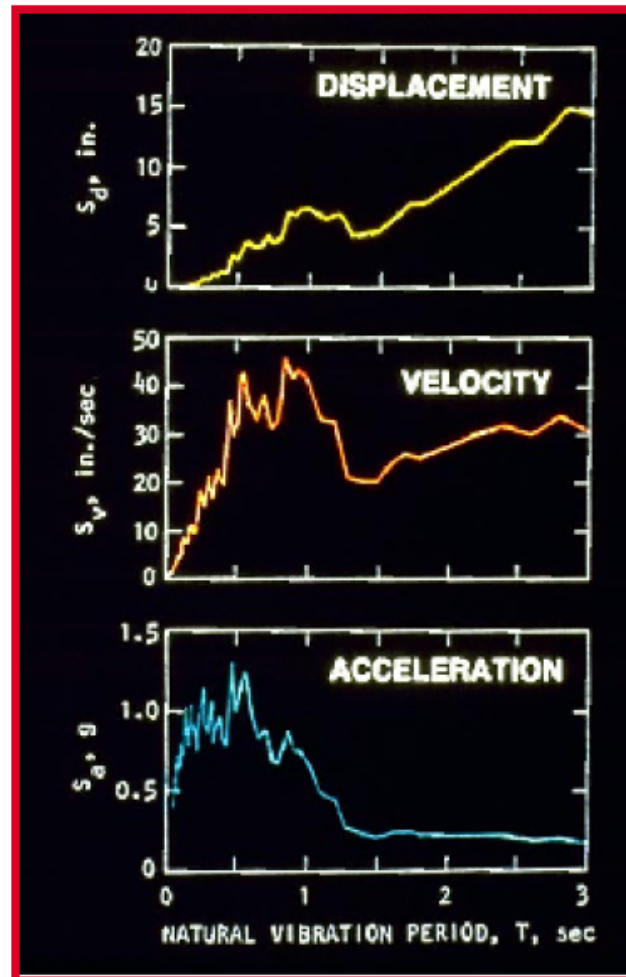
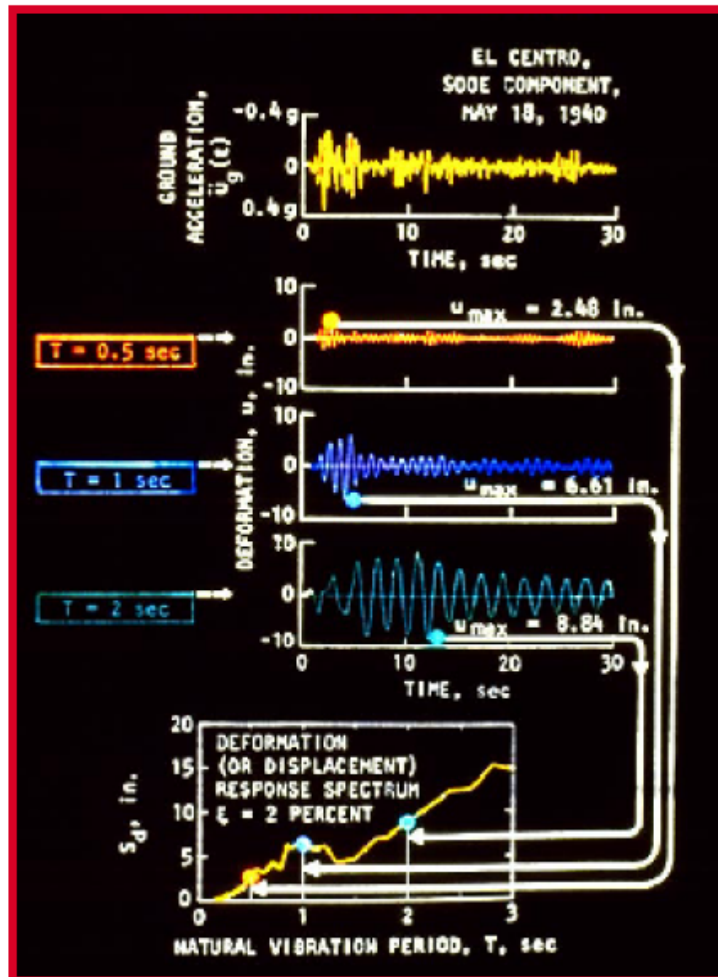
SPEC Analysis.



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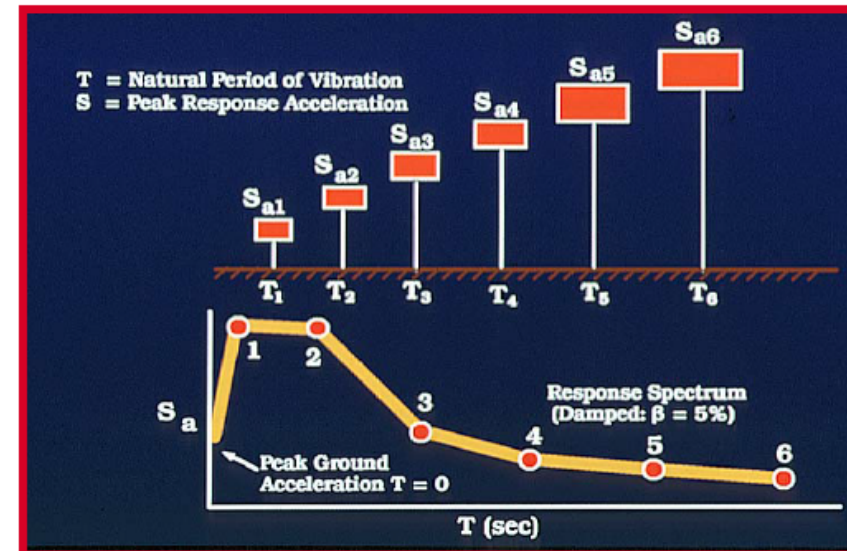
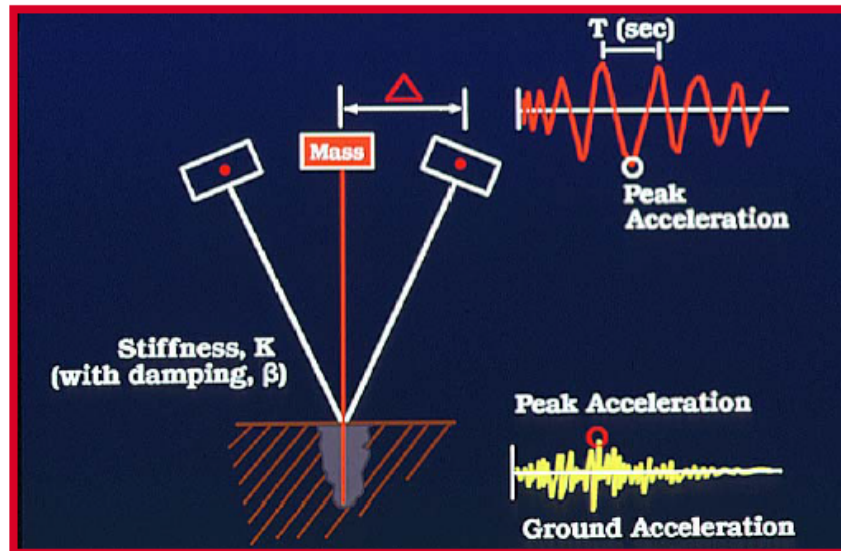
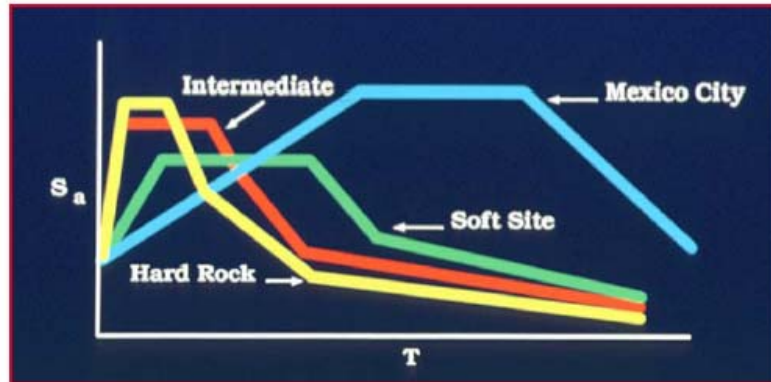
Spec Analysis Simple Theory



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Spec Analysis Simple Theory

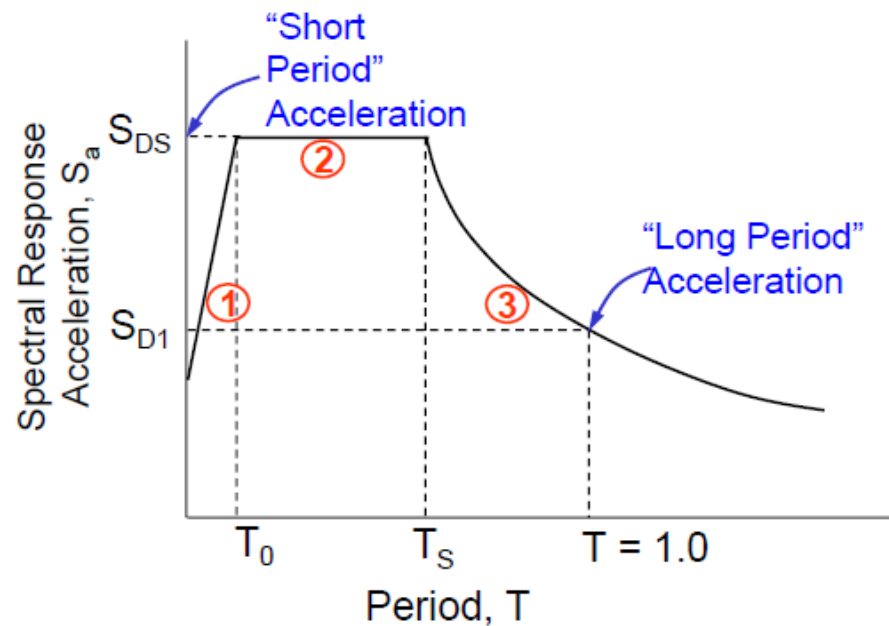


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Spec Analysis Simple Theory

ASCE 7-02 Uses a Smoothed Design Acceleration Spectrum



$$\textcircled{1} \quad S_a = 0.6 \frac{S_{DS}}{T_0} T + 0.4 S_{DS}$$

$$\textcircled{2} \quad S_a = S_{DS}$$

$$\textcircled{3} \quad S_a = \frac{S_{D1}}{T}$$

$$T_0 = \frac{0.2 S_{D1}}{S_{DS}}$$

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SDOF Simulation Program

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